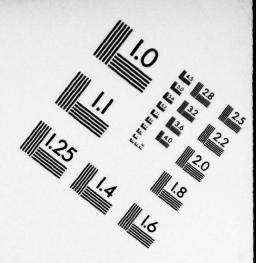
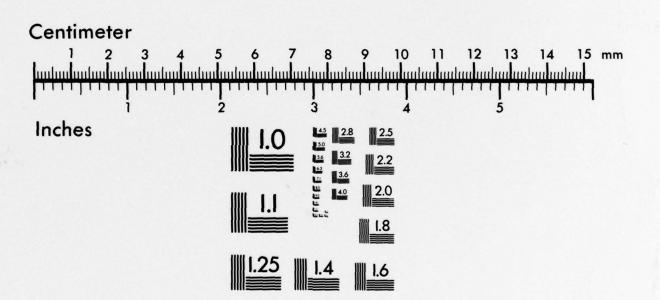


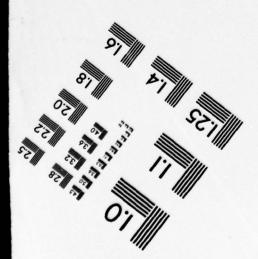


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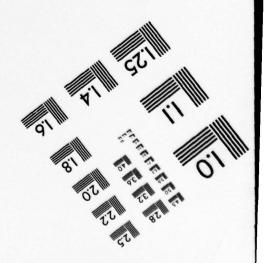
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ASC-TR-94-9296

POST TEST INFORMATION FOR THE ROCK-WELL NASP AERO PROPULSION FORCE MODEL NAPF-1

TEST (NAP-21) IN THE NASA LANGLEY 14X22 FOOT SUBSONIC TUNNEL



ALAN HEALEY NEIL BOSMAJIAN

NORTH AMERICAN AIRCRAFT ROCKWELL INTERNATIONAL CORP. PO BOX 92098 LOS ANGELES CA 90009

APRIL 1990

FINAL REPORT

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A SCALE MODEL OF A NATIONAL AERO-SPACE PLANE, A ROCKETDYNE D791-4B AIRFRAME CONFIGURATION AND THE ROCKETDYNE AFTBODY NOZZLE, WAS TESTED IN THE NASA LANGLEY 14X22 FOOT SUBSONIC WIND TUNNEL, HAMPTON, VIRGINIA, FROM 17 JANUARY 1990 TO 21 MARCH 1990. THE PURPOSE OF THIS TEST WAS TO OBTAIN POWERED GROUND EFFECTS, VEHICLE FORCES AND MOMENTS, STABILITY AND CONTROL, LOW SPEED NOZZLE PERFORMANCE, POWERED INTERFERENCE, EFFECTS ON AERODYNAMICS, CONTROL SURFACE HINGE MOMENTS, AND NOZZLE AFT BODY ACOUSTIC DATA. THESE EFFECTS WERE INVESTIGATED AT MACH 0.2. DATA WAS OBTAINED IN 440 RUNS.

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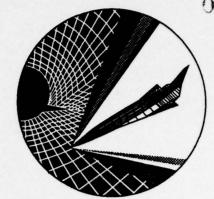
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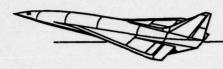
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POST TEST INFORMATION FOR THE ROCKWELL NASP AERO PROPULSION FORCE MODEL NAPF-1 TEST (NAP-21) IN THE NASA LANGLEY 14 x 22 FOOT SUBSONIC TUNNEL(U)

CONTRACT NUMBER F33657-86-C-2127

PREPARED BY

ALAN J. HEALEY
TEST SUPPORT
NATIONAL AEROSPACE PLANE

APPROVED BY

R. R. BURROWS, MANAGER WIND TUNNEL TEST NATIONAL AEROSPACE PLANE

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NATIONAL AEROSPACE PLANE

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R. R. BURROWS, MANAGER
WIND TUNNEL TEST
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Program Manager

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Rockwell International North American Aircraft Operations P.O. Box 92098 Los Angeles, California 90009 RESULTS OF THE ROCKWELL NASP AERO PROPULSION FORCE MODEL NAPF-1 TEST (NAP-21) IN THE NASA LANGLEY 14 x 22 FOOT SUBSONIC TUNNEL (U)

by

A. J. Healey

Test Support

National Aero-Space Plane

ABSTRACT

A scale model of a National Aero-Space Plane, a Rocketdyne D791-4B airframe configuration and the Rocketdyne aftbody nozzle, was tested in the NASA Langley 14 x 22 foot subsonic wind tunnel, Hampton, Virginia from 17 January, 1990 to 21 March, 1990. The purpose of this test was to obtain powered ground effects, air vehicle forces and moments, stability and control, low speed nozzle performance, powered interference effects on aerodynamics, control surface hinge moments, and nozzle aft body acoustic data. These effects were investigated at Mach 0.2. Data was obtained in 440 runs. This report does not contain any classified data or figures. For such information refer to the NASP pretest report NA 89-187 and NASA test data NASA R 90-4, both of which are located in the Rockwell NASP Technical Information Center at Downey.

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1.0 INTRODUCTION

- 1.1 (U) This document presents a summary of the NASP Aero Propulsion Force Model NAPF-1 Low Speed Ground Effects Test (NAP-21). The model, instrumentation, installation, and test conditions are described briefly, and a schedule of completed runs and anomalies are included.
- 1.2 (U) A scale model of the Rocketdyne D791-4B airframe configuration and the Rocketdyne aftbody nozzle was tested in the NASA Langley 14 x 22 subsonic wind tunnel, Hampton, Virginia. The model was shipped to Langley on January 17, 1990 and model installation in the test section began February 12, 1990. Testing began February 20, 1990 and completed March 21, 1990.
- 1.3 (U) The primary purpose of this test was to obtain powered ground effects, air vehicle forces and moments, stability and control, low speed nozzle performance, powered interference effects on aerodynamics, control surface hinge moments, and nozzle aft body acoustic data. The test also included some side slip angle runs to aid in the analysis of cross wind effects in ground effect.
- 1.4 (U) All test objectives were met. On-site preliminary analysis of the data is included in section 8.2.

1.0 INTRODUCTION (Con't)

1.5 (U) Summary:

NASA Langley 14 x 22 Foot Test Facility:

Subsonic Tunnel

372 Facility Test Number:

Test ID Number NAP-21

Installation Date: 12 February, 1990 Test Start Date: 20 February, 1990

21 March, 1990 Test Completion Date:

Test hours: 247 hours

428 hours User Occupancy Hours:

Number of Runs: 440 0.2 Mach Number

60 psf Dynamic Pressure

Angle of Attack Beta Range -4°,0° to 8°

Model: NAPF-1 (60"-scale D791-4B)

1.6 (U) The following personnel were responsible for the NASP Aero Propulsion

Force test:

Test Engineers: Alan J. Healey 213-922-0682

-4° to +16°

Neil W. Bosmajian 213-922-0026

Data Analysis: Deloy C. Olsen

Dave E. Berndt

Colin M. Mc Kinney

Mike Froehlich

Facility Test Engineers:

Greg Gatlin 804-864-5065 John Paulson 804-864-5071

- 1.0 INTRODUCTION (Con't)
- 1.7 (U) All inquires regarding this wind tunnel test program should be directed to:

Rockwell International 12214 Lakewood Blvd. Downey, California 90241 Attn: Alan Healey M/S NA 40 (213) 922-0682

2.0 REMARKS

- 2.1 (U) Table 3 is a detailed list of all known anomalies, events, and remarks regarding the model, instrumentation, data and programming during the test.
- 2.2 (U) The NASA/Langley computer was not reading the ESP pressures in their proper sequencing order which resulted in incorrect pressures being used to calculate, area pressure, and balance cavity pressure corrections. This was due to an error in the numerical sequence set up of the ESP cables to the ESP scanner box. This sequencing error was corrected and accounted for through a computer program change (Table 3 run 158).
- 2.3 (U) Numerous problems were encountered with the NASA/Langley height readout. The sector head which traverses the model up and down would slip approximately 1 to 1.5 inches when fully traversed. The height L.E.D. readout had to be zeroed every 4 to 6 runs.
- 2.4 (U) Pressure reference lines from the cannon/knuckle to the ESP modules were continually being pinched off by the blade strut cover, tight duct tape, and wire & tubing shift during test runs.
- 2.5 (U) Ambient temperature and model temperature above 105°F appeared to affect the ESP readout and zero pressure drift in the forward ESP module.
- 2.6 (U) Condensation build-up electrically grounded the metric to non-metric part of the model. A heat gun was used to dry out any remaining water. This action dried out the excess water, but inadvertently melted pressure reference lines. A complete model break down followed in order to replace the melted pressure lines.

3.0 TEST FACILITY DESCRIPTION

- 3.1 (U) The NASA Langley 14 x 22 foot Subsonic Tunnel consists of a closed circuit, single return, continuous flow atmospheric type wind tunnel and a model preparation area (MPA).
- 3.2 (U) The wind tunnel test section measures 14.5 feet high, 21.75 feet wide and approximately 50 feet long and may be configured closed with the walls in place, open with the walls and ceiling raised, and slotted with slots in the floor, ceiling, and walls. The test section floor is composed of two removable floor sections which may be a combination of model support carts, moving ground belt, or a slotted floor section. Also, floor boundary layer control is provided by a suction device in front of the first floor section. A high pressure air station and motor generators are available for model power. The test section is viewed through windows from the main control room where the tunnel and model controls are located. The test section is serviced by test site 1 which is located in a room beneath the test section.
- 3.3 (U) The model preparation area is a large, enclosed high-bay area. A high-pressure air station and a motor generator distribution box are available for powered models. A second floor control console overlooks the MPA and provides controls for the air station and motor generators. The MPA has five model interface stations hereafter called test sites (#2, #3, #4, #5, and #6) which may be shared by several models depending upon their data requirements. A model-support cart system was designed to permit models to be installed on a cart in the MPA and rolled into the wind tunnel test section fully assembled and calibrated.

3.0 TEST FACILITY DESCRIPTION (Con't)

3.4 (U) This tunnel is capable of force, moment and pressure studies. A moving belt ground plane with boundary layer suction and variable speed capabilities for operation at test section flow velocities can be installed for ground effects tests. For this test the moving belt ground plane was not used, however, the boundary layer suction device was used. A universal model support system utilizes a three joint rotary sting with +45° of pitch, +45° of yaw and 6 feet of vertical traverse. This system is mounted on a horizontal turntable with +165° of rotation. Models can be powered with either high pressure air (15 lb/sec at 5,000 psia) or variable frequency electric systems. Data are recorded with 60 channels and reduced off site.

4.0 MODEL DESCRIPTION

4.1 General

- 4.1.1 (U) The model used for this test was a 60" scaled representation of a modified Rocketdyne D791-4B airframe configuration. The model was designated as NAPF-1 and the assigned test identification code was NAP-21. The lower forebody was a representation of the Rockwell baseline vehicle D791-10R (model station 0 to 18.25, Drawing D791-10R-900), with a faired over inlet starting at model station 18.25 and continuing to the engine module. The upper fuselage surface of the model was extended outward from the baseline contour to provide the required internal area needed for the dual-flow balance and the internal nozzle flow passage. The model baseline configuration was the modified D791-4B vehicle with: flow module -601 (w/cowl flap angle δ=0°), landing gear on, nozzle flow fences on, and all control surface deflections at 0°.
- 4.1.2 (U) The model control surfaces consisted of; elevon angles of 0°, ±10°, & ±20°; body flap angles of 0°, ±10°, & ±20° and speed brake angles of ΔSB 40°, which were manually set and held in place by brackets and pins.
- 4.1.3 (U) The elevons comprise all that part of the wing panels aft of the elevon hinge line x=52.445 and outboard of butt line B.L. = \pm 3.28. The left hand elevon was gaged to obtain hinge moment data and the right hand elevon instrumented with pressure taps.
- 4.1.4 (U) One set of body flaps were fabricated out of Armco 17-4 stainless steel with three pairs of brackets to achieve the desired deflection angles (ref WT 01007-24). The brackets were reversed to obtain the negative deflections. The left hand body flap bracket was gaged for hinge moment measurements at 0° and ±20°. The ±10° deflected body flap was not gaged. Static pressure taps were located on the lower surface of the right body flap.

- 4.1.5 (U) Speed brake deflection was achieved by deflecting the elevons and body flap together. The first speed brake configuration, ΔSB 40°, was accomplished by deflecting the body flap up -20° and the elevons down +20°. The second speed brake configuration, ΔSB 20°, was not tested.
- 4.1.6 (U) The wing was constructed of Armco 17-4 stainless steel and had swept leading edge clipped delta planform with a flat lower surface which was parallel to the wing reference plane. The wing leading edge sweep was 79.5° and the dihedral angle approximately 25 degrees with +1 degree of incidence. Static pressure taps were located on the lower surface of the right wing.
- 4.1.7 (U) The mid fuselage block, model station 23.0 to 33.641, contained two pressure drop plates located at model stations 24.5 and 29.1. These pressure drop plates were used to help regulate the pressure and velocity of the internal air flow before it reached the nozzle throat. The first pressure drop plate (WT 01007-206) at MS=24.5 was 0.10 inches thick with 309 drilled holes for a total open area of 0.4691 square inches. The second pressure drop plate (WT 01007-205) at MS=29.1 was 0.10 inches thick with 309 drilled holes for a total open area of 1.047 square inches.
- 4.1.8 (U) A pair of removable nozzle flow fences were constructed out of Armco 17-4. These flow fences were mounted on the outboard edges of each side of the external nozzle just aft of the internal nozzle exit plane. The flow fences were removed to check their effectiveness in controlling lateral plume divergence.
- 4.1.9 (U) Landing configuration included one pair of main landing gear, left and right, and one nose landing gear assembly (ref drawing WT 01007-10). The wheels for the nose assembly were constructed of stainless steel and the nose gear strut of Armco 17-4. The wheels for the main gear assembly were constructed of 7075-T6 aluminum and the main gear strut of Armco 17-4.

- 4.2 Flow Modules
- 4.2.1 (U) Two interchangeable flow modules (-601 & -701) were built for this test, ref. WT 01007-6, WT 01007-7. Due to limited time and poor mating between module 701 and the external nozzle, module 701 was not tested. Both modules were made of Armco 17-4 and had 12 flow paths with 11 splitters. The flow paths were set at ±4°, ±12°, ±20°, ±28°, ±36°, and ±44°. The eleven splitters were set at 0°, ±8°, ±16°, ±24°, ±32°, ±40° with a half splitter at ±48° (Figures 1 & 2). The total nozzle throat area was 2.51797 square inches for module -601.
- 4.2.2 (U) The distinctive difference between module 601 and 701 was their cowl flap deflection angle. Flow module 601 has a cowl flap deflection angle of 0° and module 701 had an upward cowl flap deflection angle of -9°.
 - 4.3 Aft Fuselage
- 4.3.1 (U) The aft fuselage lower surface (external nozzle) was constructed modeling the Rocketdyne -4B configuration. The nozzle surface contained pressure, temperature, and acoustic instrumentation as shown in Figure 3.

5.0 INSTRUMENTATION

5.1 General

5.1.1 (U) The model was instrumented with 181 orifices to measure surface static pressures on the vehicle, but 52 of the pressure taps were eliminated as a result of NASA/Langley inability to support 48 port ESP modules. The following is a summary of those measurements that were available:

Static Pressures:	Actual	Planned	
External Nozzle:	76	102	
Upper Strut	16	22	
Right Wing	8	9	
Fuselage Side	16	20	
Flow Module - External	3	17	
Flow Module - Internal	2	3	
Elevon	2	2	
Body Flap	5	5	
Balance Cavity	1	1	
TOTAL	129	181	
Total Pressures:			
Flow Module - Internal	6	7	
Thermocouples:			
External Nozzle	0	21	
Balance Cavity	1	1	
ESP Module	1	1	
Flow Module - Internal	2	2	
Kulites			
External Nozzle	7	8	
Fuselage Side	3	3	

- 5.1.2 (U) Four 32 port ±15 psid Electronically Scanned Pressure (ESP) scanners were employed to measure all the static pressures except for the internal flow module pressures. One 32 port ±45 psid ESP scanner was used to measure 6 total pressures and 2 static pressures located in the internal flow module.
- 5.1.3 (U) Table 1 lists the correlation between the NASA/Langley numbering system and Rockwell's pressure tap numbering system and pressure tap codes.
 - 5.2 Temperature Instrumentation
- 5.2.1 (U) The 21 coaxial thermocouples located on the external nozzle were not measured during this entry. The four chromel constantan thermocouples were used to measure their respective local temperatures (see 5.1.1).
 - 5.3 Kulite Instrumentation
- 5.3.1 (U) Eleven XCE 093 series Kulites were used to obtain fluctuating pressure data. Eight of the eleven kulites were located on the external nozzle surface, but only seven of the eight were used(ref WT01007-21) Figure 3. The remaining three kulites were located on the right side of the aft fuselage (ref WT 01007-21). These data were recorded on a facility-supplied FM tape recorder using WB group I at 60 ips, with a frequency response DC to 40 KC. The center frequency was 216 KHz.
 - 5.4 Strain Gage Instrumentation
- 5.4.1 (U) Hinge moments were obtained from 350 ohm strain gage bridges mounted on the brackets of the left body flap and on the shaft of the left elevon.
- 5.4.2 (U) The 0°, +20°, & -20° brackets of the body flap were gaged with a bending strain gage model WK-06-06TW-350. The ±10° brackets were not gaged. The hinge line for the body flap is at model station 56.704.
- 5.4.3 (U) The left elevon was gaged at its shaft with a torsion strain gage to obtain hinge moment data at 0° , $\pm 10^{\circ}$, & $\pm 20^{\circ}$. The hinge line for the elevons is at model station 52.455.

6.0 MODEL INSTALLATION

- 6.1 (U) The model was strut mounted and was designed to obtain nozzle thrust minus drag data, fuselage aftbody force and moment data in the presence and absence of simulated engine exhaust flow. A 47.750° swept strut was attached to the aft end of the model in the vertical tail location. The model was mounted upright on the strut (Figure 4). The strut contained a flow-through duct to channel high pressure air to the model for nozzle exit flow simulation and a separate duct for model instrumentation (ref. WT01007-15). The strut in turn was attached to Rockwell's supplied strut adaptor which was connected to NASA/Langley's long cannon via a NASA supplied knuckle and roll coupling.
- 6.2 (U) Two knuckles were employed to cover the required angle of attack range. The first installation (Figure 4) covered the lower pitch angles from -4° to +12° while the second assembly, the 24° knuckle, provided for the higher range of 12° to 16°. The second assembly had the roll coupling mounted after the 24° knuckle.
- 6.3 (U) The General Dynamics/Convair Division C-15-2.5 A-I Dual Flow-Through 6-Component Force Balance was fixed to the strut with two push-on screws, and held in roll by a roll pin. The balance adapter was slipped over and pinned to the balance. The upper aft fuselage was then mounted on the balance assembly and pinned to the adapter. A grounding strip was affixed around metric gap.
- 6.4 (U) The dimensions of the General Dynamics/Convair Division C-15-2.5 A-I Dual Flow-Through 6-Component Force Balance, geometry relating the model reference center and the balance center can be found in reference NA 89-187.

- 6.0 MODEL INSTALLATION (Con't)
- 6.5 (U) All electrical cables and reference pressure tubes were routed from the model through the blade strut and out the strut adaptor along the long canon down tunnel support to the electrical patchboard located below the test section. The one inch high pressure air supply line was also routed to the same area and connected to the tunnel high pressure supply system. To guard against the turbulence caused by the nozzle exhaust and general air flow, the bundles of cables and tubes were tape wrapped to the strut adaptor and long canon.

7.0 TEST CONDITIONS & PROCEDURES

- 7.1 (U) The NAP-21 test was conducted at a constant Mach number of 0.2 and a dynamic pressure of 60 psf. Two dynamic pressure sweeps from 0 to 80 psf were performed to confirm that the Re effects on drag were stable at 60 psf.
- 7.2 (U) The test variables included elevon deflection; 0°, ±10°, ±20°, body flap deflections; 0°, ±10°, ±20°, speed brake deflections, NPR settings; 75%, 82%,100%, 112%, 125%, angle of attack; -4°, 0°, 4°, 8°, 12°, 16°, Beta; -4°, 0°, 4°, 8°, nozzle flow fences on & off, and landing gear on & off. Data were obtained for all test variables.
- 7.3 (U) The GD C-15-2.5 A-I balance was completely calibrated up to maximum load capacity in July 1989 at GD's Convair Division in San Diego. A tape of the balance calibration matrix in NASA/Langley format including, interactions, pressure tares, etc., was sent to NASA/Langley. NASA/Langley performed a series of balance check loads to verify the GD calibration matrix.
- 7.4 (U) In-tunnel check loadings of the balance through the facility's data acquisition system was performed after installation to ensure the integrity of the total force and moment measurement system.
- 7.5 (U) Internal nozzle thrust tare calibrations for each NPR setting was conducted prior to testing. Mass flow measurements, balance supply pressure and nozzle pressure measurements were recorded for each data point. For these thrust tares, wing, body flap and external nozzle were removed from the model and the external nozzle was replaced with a non-metric shield to avoid jet impingement on the model.
- 7.6 (U) A complete hinge moment calibration was performed prior to the test at the Rockwell NAA Calibration Facility (ref WTL-090-4). In-tunnel check hinge moment loads were performed through the facility data system.

7.0 TEST CONDITION & PROCEDURES (Con't)

- 7.7 (U) Air pressures required for this test depended upon the NPR. The 75%, 100%, & 125% NPR corresponded to predicted nozzle throat pressures of approx. 31, 41 and 51psia. Balance supply pressures were set at 168, 228 and 288 psia to obtain the desired Ptn. The corresponding mass flow rate for the 75%, 100% & 125% NPR settings were approximately 1.659, 2.212 and 2.765 lb/sec, respectively.
- 7.8 (U) The height variation for the ground effect testing was varied from wheels on ground (one inch above) to tunnel center line. h/L checks were made every opportunity the tunnel test section was open at which time the height L.E.D. was corrected.
- 7.9 (U) Using the required Mach number and dynamic pressure setting, a height sweep was performed for each configuration and power setting, including power off.
- 7.10 (U) The specific combinations of runs number, Mach number, model configuration, orientation, and control surface deflections are shown in the run log, Table 2

8.0 DATA PROCESSING

- 8.1 (U) Magnetic data tapes and tabulated printed data, NASA Langley Report R-90-4 books 1 thru 32, are available at the Rockwell NASP TIC. Observations and data analysis from the propulsion group and aerodynamics group are still pending.
- 8.2 (U) All test objectives were met. On-site preliminary analysis of the data indicates the following:
 - Stability axis data showed that increasing NPR increases pitching moment and decreases lift. The decrease in lift is attributed to the base drag increase and the change in the stream thrust vector angle.
 - Application of power produces a large positive pitching moment and increased lift at high angles of attack which would aid takeoff and landing characteristics.
 - 3. Ground effect causes a suction effect at low attitudes and increased lift at takeoff angles of attack.
 - 4. Unpowered body flap effectiveness shows excellent agreement with analytical estimates. Body flap control is significantly enhanced due to addition of power and in the presence of the ground (Figure 6, Alpha = 14°; Figure 7, Alpha = -4°).
 - 5. Elevon effectiveness was slightly increased due to plume impingement.
 - 6. Internal model flow system non-uniformities were encountered at total pressure tap #A3 during the entire test. This total pressure tap lies on the splitter between nozzle 4 and 5 in the internal nozzle as shown in Figure 1. This pressure spike of 2 to 4 psi caused a yawing moment and a non-uniform pressure distribution on the external nozzle surface. This anomaly requires additional analysis and may require a flow field survey of the nozzle exit plane to fully characterize the exit conditions

8.0 DATA PROCESSING (Con't)

7. The row of external nozzle static pressures that are in line with the center line of nozzle 7, see 'a' of Figure 3, indicates lower pressures than those in line with the center line of the splitters to either side of nozzle 7 (see 'b').

9.0 TEST MATRIX

9.1 (U) Table 2 is a list of all the wind-on and static runs for the NAPF-1 model at NASA/Langley 14 x 22 tunnel. From the planned 636 runs (reference NA-89-187), 440 runs were completed. Of those 440 runs, 71 were repeated for various reasons. Since Kulite data and pressure data could not be taken at the same time, several key runs were repeated to obtain the acoustic data. Other runs were repeated when it was discovered that reference pressure tubes were pinched. A number of baseline runs were repeated in order to check the validity of the data acquisition method, and to insure data repeatability. The runs eliminated from the original run schedule due to time constraints were 32 alternate cowl runs, 32 Δ20° speed brake runs, and various angles of attack, power settings and betas runs.

10.0 CONCLUSION

- 10.1 (U) All objectives stated in the Pretest Information Report NA-89-187 have been achieved:
 - 1. Powered and unpowered ground effects
 - 2. Low speed nozzle performance
 - 3. Powered interference effects on aerodynamics
 - 4. Control surface hinge moments
 - 5. Vehicle force and moment & stability and control

Further analysis will provide nozzle and plume flow definition, configuration effects, and more detailed control surface effectiveness.

11.0 REFERENCES

11.1	(U)	NA89-187	"Pretest Information for the Rockwell NASP Aero Propulsion Force Model NAPF-1 Test (NAP-21) in the NASA Langley 14 x 22 Foot Subsonic Tunnel (U)" November 1989.
11.2	(U)	NA89-116	"Structural Analysis of the NASP Aft Body Plume Wind Tunnel Model (NAPF-1)" April 1989.
11.3	(U)	NASA R90-4	"NASA Langley Magnetic and Tabulated Data" April 1990.
11.4	(U)		"14 x 22 Foot Subsonic Tunnel Test Engineer's Manual" March 1988.
11.5	(U)		"User's Manual for the Langley Research Center 14 x 22 Foot Wind Tunnel Facility Data Acquisition System" September 1987.

12.0 TABLES

Table 1 Pressure Tap Numbering System

Table 2 NAPF-1 NASA/Langley 14 x 22 Run Schedule

Table 3 Test Notes and Anomalies

Pressure Tap Numbering System

NASA /LANGLEY	-	Beta≃0		
Computer	Tap #	Code	Location	Comments
Print Out #'s	100 e	Code	Location	Comments
1	1	N1,01	External Nozzle	
2	2	N1,02	Nozzle 12 Exit Static	
3	4	N1.04	Nozzle 11 Exit Static	
4	5	N1,06	Nozzle 10 Exit Static	
5	6	N1,08	Nozzle 9 Exit Static	
6	8	N1,10	Nozzle 8 Exit Static	
7	10	N1,12	Nozzle 7 Exit Static	
8	11	N1.13	External Nozzle	
9	12	N1.14	Nozzle 6 Exit Static	
10	13	N1,16	Nozzle 5 Exit Static	
11	14	N1,18	Nozzle 4 Exit Static	
12	15	N1,20	Nozzle 3 Exit Static	
13	16	N1,22	Nozzle 2 Exit Static	
14	17	N1,24	Nozzle 1 Exit Static	
15	18	N1,25	External Nozzle	
16	19	N2.01	External Nozzle	
17	23	N2.12	External Nozzle	
18	24	N2.12	External Nozzle	
19	25	N3.01	External Nozzle	
20	27	N3,12	External Nozzle	
21	28	N3.12	External Nozzle	
22	29	N4.01	External Nozzle	
23	32	N4.06	External Nozzle	
24	36	N4.12	External Nozzle	
25	37	N4.13	External Nozzie	
26	38	N4.20	External Nozzie	
27	39	N4.25		
28	40	N5.01	External Nozzle External Nozzle	
29	42	N5.12	External Nozzie	
30	43	N5.13	External Nozzle	
31	44	N6.01	External Nozzle	
32	47	N6.06	External Nozzle	
97	108	\$1,6	Upper Strut	
98	109	\$1,9	Upper Strut	
99	110	\$2.5	Upper Strut	
100	111	S2.10	Upper Strut	
101	112	\$3.2	Upper Strut	
102	117	S3,13	Upper Strut	
103	118	S4.6	Upper Strut	
104	119	S4.9	Upper Strut	
105	120	S5.6	Upper Strut	
106	121	S5.9	Upper Strut	
107	122	S6.1	Upper Strut	
	1			
109	124	S6.5 S6.7	Upper Strut Upper Strut	
110	126	S6.8	Upper Strut	
111	127	S6,10	Upper Strut	
112	129	S6.14	Upper Strut	
113	130	W1.1		
			Lower Right Wing	
114	131	W2.1	Lower Right Wing	
115		W2.2	Lower Right Wing	
116	133	W3.1	Lower Right Wing	
117	134	W3.2	Lower Right Wing	
118	143	BC WE 4	Balance Cavity	
119	136	W5.1	Lower Right Wing	
120	137	W5.2	Lower Right Wing	
121	138	W5.3	Lower Right Wing	
122	139	W6,1	Lower Right Wing	
123	140	W6.3	Lower Right Wing	
124	149	SR6.3	Right Side of Flow Module	
125	152	SR7,3	Lower Right Wing	
126	155	SR8.3	Lower Right Wing	

IASA /LANGLEY	-			
Computer	Tap #	Code	Location	Comments
Print Out #'s	1			
127	157	SR9.2	Lower Right Wing	10. 10. 100.
128	160	SR10.3	Lower Right Wing	After run 449 tap160 became a reference line pressure
33	49	N6.10	External Nozzle	
34	50	N6.12	External Nozzle	
35	51	N6.13	External Nozzle	
36	52	N6.20	External Nozzle	
37	53	N6.25	External Nozzle	
38	54	N7.01	External Nozzle	
39 40	57	N7.06	External Nozzle	
41	60	N7.10 N7.12	External Nozzle External Nozzle	
42	61	N7.13	External Nozzle	
43	62	N7.20	External Nozzle	
44	63	N7,25	External Nozzle	
45	64	N8,01	External Nozzle	
46	65	N8.06	External Nozzle	
47	66	N8,10	External Nozzle	
48	67	N8.12	External Nozzle External Nozzle	
49	68	N8,12	External Nozzle	
50	69	N9.01	External Nozzle	
51	71	N9.06	External Nozzle	
52	73	N9.10	External Nozzle	
53	74	N9.13	External Nozzle	
54	75	N9.20	External Nozzle	
5.5	76	N9,25	External Nozzle	
56	77	N10,13	External Nozzle	According the Nozzle group this tap was not reading correctly
57	141	SR1,1	Right Side of Flow Module	According the Nozzie group this tap was not reading correctly
58	142	SR2,1	Right Side of Flow Module	
	open	OHE.I	open	After run 449 this open tap became a reference line pressure
60	144	SR3,1	Right Side of Flow Module	Anter full 443 this open tap became a reference line pressure
61	145	SR4.1	Right Side of Flow Module	
62	178	FO1	Center Line on Flow Module	
63	179	FO2	Center Line on Flow Module	
64	180	FO3	Center Line on Flow Module	
6.5	78	N11,01	External Nozzle	
66	79	N11,06	External Nozzle	
67	81	N11,13	External Nozzle	
68	82	N11,20	External Nozzle	
69	83	N11,25	External Nozzle	
70	84	N12,13	External Nozzle	
71	85	N13,01	External Nozzle	
72	86	N13.06	External Nozzle	
73	88	N13,13	External Nozzle	
74	89	N13,20	External Nozzle	
75	90	N13,25	External Nozzie	
76	91	N14,13	External Nozzle	
77	92	N15,01	External Nozzle	
78	93	N15.06	External Nozzle	
79	95	N15.13	External Nozzle	
80	96	N15.20	External Nozzle	
81	97	N15,25	External Nozzle	
82	98	N16,13	External Nozzle	
83	101	N18.13	External Nozzle	
84	102	N18.20	Body Flap	
85	103	N18,25	Body Flap	
86	104	N19.13	External Nozzle	
87	105	N19.16	Body Flap	
88	106	N19,20	Body Flap	
89	107	N19,25	Body Flap	
90	146	SR5,1	Right Side of External Nozzle	After run 449 tap146 became a reference line pressure
91	148	SR6.2	Right Side of External Nozzle	
92	150	SR7.1	Right Side of External Nozzle	
32				

Table 1 Pressure Tap Numbering System

NASA /LANGLEY				
Computer	Tap #	Code	Location	Comments
Print Out #'s				
94	156	SR9.1	Right Side of External Nozzle	
95	159	SR10.1	Right Side of External Nozzle	
96	161	SR11.2	Right Side of External Nozzle	
129	181	_A1	Tot. Pres. Radius 4.483 (Rt)	
130	182	A2	Rad deg = 32	
131	183	A3	Rad deg = 16	
132	184	A4	Rad deg = 0	
133	185	A5	Rad deg = -16	
134	186	A6	Rad deg = -32	
135	187	A7	Tot. Pres. Radius 4.483 (Lft)	
	open		open	
137	176	DS1	Primary Flow Static	
138	177	DS2	Primary Flow Static	
	178	No DS3	Primary Flow	

Table 2 NAPF-1 NASA/Langley 14 x 22 Run Log

Gear Comments	on Zero Thrust runs, 150 psi to 350 psi A50psi, #1 upper lett	on Zero Thrust runs, 150 psi to 350 psi A50psi, #1 lower left	on Zero Thrust runs, 150 psi to 350 psi A50psi, #1 lower right	on Zero Thrust runs, 150 psi to 350 psi ∆50psi, #1 upper right	uo	on Static Thrust Run for Landing Gear Effectiveness	vo	uo	ио	uo	on Q Sweep, 0 to 80 psf AQ=10psf, on Tunnel Cener Line	on Q Sweep, 0 to 80 psf AQ=10psf, on Tunnel Cener Line	on Upper Limit was 64.134"	on Upper Limit was 81,309"	on Lower Limit was 21.934	on Lower Limit was 57.774	on Bad ESP Data, Good Balance Data	Run Number Skipped	on Repeat of 92	on Repeat of 93	on Repeat of 94	on Repeat of 95	on Weight Tares	No Final Zero, h/L came off line	on Repeat of Run 95	uo	on Repeat of 99	on 20 min alpha = 4, Fixed ESP Interface Box, Repeat of Run 99					
F.F. G	6	5	6	6	uo		6	ы	6	6	6	0	6	6	6	6	6	6	6	6	6	uo		6	6	6	6	uo		uo	LO	uo	ou
Æ	1.5x10 6	1.5x10 6	1.5×10 6	1.5x10 6	1.5x10 6	1.5x10 6	0	0	0	0			1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6		1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5×10 6		1.5x10 6	1.5×10 6	1.5x10 6 o	1.5x10 6 o
νc	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		0	0	0	0	0		0	0	0	0
_	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		0	0	0	0	0		0	0	0	0
Δelv	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		0	0	0	0	0		0	0	0	0
h/LK Data Aelv Abf													Yes	Yes	Yes	Yes	2	2	2	2	2	2		2	2	2	2	2		2		2	2
Beta Beginning h/l											81.284"	81.284	8.2	6.65	22.617"	2.7	59.394"	23.656"	6.6575	8.2486"	6.6499"	6.6162"		0.1371	0.1106	0.377	0.9756					0.1369	0.137
Beta						0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		0	0	0	0			0	0	0	0
Alpha						0	0	0	0	0	0	12	1-4	0	4	12	12	4	0	4.	0	0		4.	0	4	12		4	12	80	4.	0 4-
PBEL							168	187	227	288	0	0	0	0	0	0	168	168	168	168	187	255		0	0	0	0			0	0	168	168
o							0	0	0	0	Sweep	Sweep	09	09	9	09	9	09	09	09	09	09		09	09	09	09			09	09	09	09
Date	20-Feb	20-Feb	20-Feb	20-Feb		21-Feb					22-Feb S	22-Feb S	22-Feb	22-Feb	22-Feb	22-Feb	22-Feb	22-Feb	22-Feb	22-Feb	22-Feb	22-Feb		23-Feb	23-Feb	23-Feb	23-Feb	23-Feb	23-Feb	23-Feb	23-Feb	23-Feb	23-Feb
nd Time				22:17								,,,	. 4	.,	,,,		17:50	18:04	18:27	18:43	19:00	19:20		,4	,,4	,,	(4	.4	,,	(4	14	17:02 2	21:10 2
Start Time End Time	20:05	20:55	21:35	22:00													17:45	17:50	18:04	18:27	18:43	19:00		9:50	10:14	11:00	11:10			15:50		16:46	20:50
Run #	30	81	82	83	84	85	98	87	88	89	90	91	92	93	94	95	96	97	86	66	100	101	102	103	104	105	106	107	108	109	110	=	112

Table 2 NAPF-1 NASA/Langley 14 x 22 Run Log

	1	1	1	T			T			1	1	1			T														
Gear Comments	on 29 min alpha=0, Repeat of Run 113	n 14 min alpha=4, Repeat of Run 97	n 8 min alpha=8	n 7 min alpha=12, Repeat of Run 96	on 20 min, Repeat of Run 100	on 24 min, Repeat of Run 101	on 65.833"	n 82.384"	n 84.066"	n 40.033 to 84.046	n 57.915 to 84.045	n 57.866 to 84.028	on 39,906 to 84.003	on 22.362 to	n 6.644 to81.8	on 8.2036 to 64.833	on 58.749 to 84.017 Nose Right	on 8.2005 to 65.736 Nose Left	on 6.6554 to	on 22.652 to 84.052	on 39.826 to 84.014	n 57.688 to 84.031	on 57.6 to 84.064	on 39.66 to 84.066	n 22.6 to	on 6.6644 to 81,495	on 8.2769 to 65.730	on 8.2937 to 65.562	on 6.6666 to 82.340
F.F. G	o uo	o uo	uo uo	uo uo	o uo	6	6	uo uo	no no	o uo	uo uo	uo uo	o uo	o uo	uo uo	6	о 10	6	0	0	0	ю	0 6	0	o uo	6	0	0 10	o uo
\forall	-	-	-	-	-	_	-	-	-	9	-	-	-	-	-	_	_	_	-	9	_	-	_	-	9		-	9	\dashv
Æ	1.5×10 6	1.5×10 6	1.5×10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5x10	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10	1.5×10 6	1.5×10 6	1.5×10	1.5×10 6
ΔC	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	٥	0	0	0	0	0	0	0	0	0	0	0	0	0
ADI	0	0	0	0	0	0	٥	0	0	0	0	0	0	0	0	٥	٥	٥	0	0	٥	0	0	0	0	0	0	0	0
a del	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	٥	0	0	0	0	0	0	0	0	0	0	0
h/LK Data delv abf	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2
Beta Beginning h	0.1108	0.3887	0.6801	0.9749	0.1108	0.1105	0.1376	0.1107	0.3766	0.6672	0.9653	0.9644	0.6651	0.3727	0.1107	0.1367	0.9792	0.1367	0.1109	0.3775	0.6638	0.9615	0.9598	0.6638		0.1111	0.1379	0.1382	0.1111
Beta	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	4	4	4	4	4	4	4	4	4	4	4	4
Alpha	0	,	80	12	0	0	- 4	0	*	80	12	12	80	•	0	4	12	4-	0	4	80	12	12	60	4	0	4.	4	0
PBEL	168	168	168	168	187	255	228	228	228	228	228	288	287	290	289	287	0	290	291	288	288	288	229	229	228	228	228	168	176
o	60	9	60	9	9	60	9	60	60	60	60	60	9	60	60	9	90	60	9	9	9	9	90	9	90	9	9	9	9
Date	23-Feb	23-Feb	23-Feb	23-Feb	23-Feb	23-Feb	26-Feb	26-Feb	26-Feb	26-Feb	26-Feb	26-Feb	26-Feb	26-Feb	26-Feb	26-Feb	26-Feb	26-Feb	26-Feb	26-Feb	26-Feb	26-Feb	26-Feb	26-Feb	26-Feb	26-Feb	27-Feb	27-Feb	27-Feb
End Time	21:45	22:03	22:13		22:50	_	15:11	15:40		16:05	16:10	_	16:27	16:42	17:10	17:34	20:23	20:46	21:23	21:34	21:44	21:50	21:59	22:08	22:21	22:47	8:23	5:46	10:25
Run # Start Time End Time	21:16	21:49	22:05	22:17	22:30	22:56	14:58	15:17	15:43	15:57	16:05	16:14	16:20	16:32	16:46	17:20	20:16	20:30	20:55	21:24	21:40	21:46	21:55	22:02	22:12	22:30	8:08	8:28	9:59
Run #	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141

168=75% 228=100% 288=125%

AJH

Table 2 NAPF-1 NASA/Langley 14 x 22 Run Log

				T				П	T										_								
Gear Comments							Repeat of Run 120	Kulite Data No Good, Repeat of Run 128	on Kulite Data No Good, Repeat of Run 127	Kulite Data No Good, Repeat of Run 126	Kulite Data No Good, Repeat of Run 121	Kulite Data No Good, Repeat of Run 120	Kulite Data No Good, Repeat of Run 119	Kulite Data No Good, Repeat of Run 99	on Kulite Data No Good, Repeat of Run 98	Kulite Data No Good, Tape ran out, Repeat of Run 97	Static runs for Body Flap Effectiveness	Static runs for Body Flap Effectiveness	Static runs for Body Flap Effectiveness	M=0.2, Q=60psf		Before run 163 changed ESP numbering, Still questionable!					AJH
Gear	8	6	6	8	vo	6	8	8	6	8	6	8	8	6	6	6	8	8	6	uo	Б	6	6	6	ю	on	
F.F.	uo	6	6	6	ou	6	6	uo	6	6	6	ю	6	6	uo	6	ю	6	uo	uo	6	6	uo	uo	uo	on	
Æ	1.5×10 6	1.5×10 6	1.5x10 6	1.5x10 6	1.5×10 6	1.5x10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5x10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	0	0	0	1.5×10 6	1.5×10 6	1.5x10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	
νc	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-10	-10	-10	10	-10	10	10	-10	10	.10	
Aelv	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
K Data	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	
Beta Beginning h/LK DataΔelv Δbf	0.3801	0.669	0.6681	0.3775	0.1108	0.1369	0.111	0.1377	0.1113	0.3834	0.3814	0.1106	0.1374	0.1368	0.1109	0.3739	0.111	0.111	0.111	0.1371	0.111	0.3887	0.6791	0.6793	0.3891	0.111	288=125%
Beta	4	4	4	4	4	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Alpha	4	8	8	4	0	4.	0	4.	0	4	4	0	4.	4.	0	4	0	0	0	. 4	0	4	8	8	4	0	6 228-100%
PBEL	170	167	0	0	0	0	229	288	288	288	228	228	228	166	166	166	288	227	168	168	168	168	168	228	228	228	168=75%
0	09	60	09	9	60	09	9	09	09	9	09	09	09	09	09	9	0	0	0	09	9	09	09	9	09	09	
Date	27-Feb	27-Feb	27-Feb	27-Feb	27-Feb	27-Feb	27-Feb	27-Feb	27-Feb	27-Feb	27-Feb	27-Feb	27-Feb	27-Feb	27-Feb	27-Feb	27-Feb	27-Feb	27-Feb	27-Feb							
End Time	10:39	10:43	10:52	11:04	11:35	11:51	13:20	13:49	14:03	14:08	14:18	14:28	14:41	14:52	15:06		17:40	18:05	18:25	18:48	19:10	21:16	21:20	21:28	21:35	21:58	
Start Time End Time	10:29	10:40	10:48	10:57	11:09	11:37	13:00	13:38	13:54	14:05	14:13	14:20	14:33	14:44	14:57	15:08	17:22	17:46	18:08	18:35	18:53	21:09	21:18	21:23	21:29	21:40	
Run #	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	

Table 2 NAPF-1 NASA/Langley 14 x 22 Run Log

Gear Comments										Repeat of Run 95	Repeat of Run 93	2 data points - short cals, Repeat of Run 95	short cals prior to every point, Repeat of Run 86	ESP reference on PA!! static runs, Repeat of Run 86	Repeat of Run 87	Repeat of Run 88		Repeat of Run 89	repeat of baseline, Repeat of Run 92	Repeat of Run 93	Repeat of Run 98	Repeat of Run 99	Repeat of Run 100	Baseline Reruns, Repeat of Run 101	Repeat of Run 119	Repeat of Run 120	HCA
	8	6	8	8	8	6	5	6	8	8	6	6	5	6	8	6	5	6	6	6	8	6	6	6	6	o	
F. F.	8	5	8	8	8	6	8	8	8	8	8	8	5	5	8	8	8	8	5	6	8	6	8	8	6	o	
Æ	1.5×10 6	1.5×10 6	1.5x10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	0	0	0	0	0	0	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	
ΔC	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Δbf	-10	-10	-10	-10	-10	-10	-10	-10	-10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Aelv	0	0	0	0	0	0	0	0	0	٥	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
h/L K Data Delv Abf	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	
Beta Beginning h/L	0.1373	0.137	0.111	0.3892	0.6653	0.6778	0.3856	0.111	0.1367	E	min	min	0.111	0.111	0.111	0.111	0.111	0.111	0.1368	0.1097	0.1107	0.1369	0.1116	0.1109	0.1372	0.1114	288=125%
Beta	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Alpha	4.	4.	0	4	8	8	4	0	7.	12	0	12	0	0	0	0	0	0	4.	0	0	4.	0	0	4.	0	100
PBEL	228	288	288	288	288	0	0	0	0	0	0	0	168	169	187	231	255	288	0	0	168	168	187	255	229	229	168=75%
a	9	09	09	60	60	9	9	60	60	60	60	60	0	0	0	0	0	0	9	9	9	9	9	9	9	09	
Date	27-Feb	27-Feb	27-Feb	27-Feb	27-Feb	28-Feb	28-Feb	28-Feb	28-Feb	28-Feb	28-Feb	28-Feb	1-Mar	1-Mar	1-Mar	1-Mar	1-Mar	1-Mar	1-Mar	1-Mar	1-Mar	1-Mar	1-Mar	1-Mar	1-Mar	1-Mar	
End Time	22:10		_	23:06			9:29	9:53	10:14	21:05	21:35	23:07	9:00	11:32	11:55	13:13	13:37	14:20	14:34	15:05	15:31	15:48	16:15	17:49	18:14	18:35	
Start Time End Time	21:59	22:17	22:30	22:58	23:08	9:19	9:23	9:34	9:55	20:50	21:10	22:39	8:00	11:10	11:40	12:50	13:15	13:43	14:20	14:37	15:07	15:33	15:54	17:29	18:01	18:20	
Run *		169	170	171	172	173	174	175	176	177	178	179	180	181	182	183	184	185	186	187	188	189	190	191	192	193	

Table 2 NAPF-1 NASA/Langley 14 x 22 Run Log

Gear Comments	on Repeat of Run 127	on Completes Bseline reruns at Beta=0°, Repeat of Run 128	on Moved Pitot probe , Repeat of Run 131	on Repeat of Run 130	on Repeat of Run 139	on Repeat of Run 138	on Repeat of Run 141	on Est 5 days to knuckle change, Repeat of Run 140	on Repeat of Run 147	on Repeat of Run 146	on Static Runs body flap -20°	uo	uo	on Wind on BFE	uo	uo	on Bad HMBF Reading, Channel 25 was hooked into channel 34	on Bad HMBF Reading, Channel 25 was hooked into channel 34	on Point 10 was a bad point, low Pbel	on Bad HMBF Reading, Channel 25 was hooked into channel 34	on Bad HMBF Reading, Channel 25 was hooked into channel 34	on Bad HMBF Reading, Channel 25 was hooked into channel 34	on Bad HMBF Reading, Channel 25 was hooked into channel 34	on Had to rewind tape	on Bad HMBF Reading, Channel 25 was hooked into channel 34	on Bad HMBF Reading, Channel 25 was hooked into channel 34	HCA
F.F.	5	6	6	6	uo	6	5	6	6	6	ь	uo	6	6	- Lo	ь	uo	6	uo	uo	6	6	6	Lo	6	ou	
Æ	1.5x10 6	1.5×10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	0	0	0	1.5x10 6	1.5×10 6	1.5x10 6	1.5×10 6	1.5x10 6	1.5x10 6	1.5×10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	
D C	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Abf	0	0	0	0	0	0	0	0	0	0	-20	-20	-20	-20	-20	-20	-20	-20	-20	-20	-20	-20	-20	-20	-20	-20	
Λειν	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
h/L K DataΔelv Δbf Δ c	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	
Beta Beginning h/l	0.111	0.1367	0.1059	0.1368	0.1368	0.111	0.1107	0.1108	0.1378	0.1108	0.111	0.111	0.1107	0.6735	0.3819	0.1113	0.1388	0.1365	0.111	0.3819	0.3819	0.1203	0.1368	0.1368	0.111	0.3885	288=125%
Beta	0	0	4	4	4	4	4	4	4	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Alpha	0	4-	0	4.	4.	0	0	4-	4.	0	0	0	0	8	4	0	- 4	4	0	4	4	0	4.	4.	0	4	228-100%
PBEL	287	286	288	288	228	228	168	168	0	0	168	230	288	0	0	0	0	288	288	288	228	228	228	168	168	168	168=75%
o	9	9	9	9	9	9	9	9	9	9	0	0	0	09	9	09	09	09	09	09	09	09	09	09	09	60	
Date	1-Mar	1-Mar	1-Mar	1-Mar	1-Mar	1-Mar	1-Mar	1-Mar	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	
nd Time	19:01	19:17	21:46	22:03	22:20	22:42	23:03	23:24	8:10	8:34	10:01	10:35	11:03	11:12	11:20	11:45	14:37	14:54	15:14	15:36	16:00	16:21	16:38	17:52	18:15	18:26	
Start Time End Time	18:41	19:06	21:29	21:51	22:09	22:25	22:49	23:08	7:59	8:14	9:43	10:10	10:37	11:10	11:14	11:25	14:27	14:46	14:59	15:14	15:41	16:07	16:25	17:40	17:58	18:20	
Run *	194	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210	211	212	213	214	215	216	217	218	219	

Table 2 NAPF-1 NASA/Langley 14 x 22 Run Log

Gear Comments	Q code = 0 BFE static run +20°	Bad HMBF Reading, Channel 25 was hooked into channel 34	Bad HMBF Reading, Channel 25 was hooked into channel 34	Runs 223 and 224 ran together	Bad HMBF Reading, Channel 25 was hooked into channel 34	contains a void point	Bad HMBF Reading, Channel 25 was hooked into channel 34	Bad HMBF Reading, Channel 25 was hooked into channel 34	Bad HMBF Reading, Channel 25 was hooked into channel 34	Repeat of run 227 Includes weight tares, Fixed HMBF	Repeat of run 228							Speed Brake Static Runs			Speed Brake Effectiveness						AJH
	8	8	5	8	8	6	8	8	8	5	5	8	5	5	8	5	6	6	6	6	6	6	8	6	6	Ю	
n. R.	8	5	8	8	5	6	8	8	5	8	6	8	5	8	5	8	5	6	6	5	6	6	6	Б	6	6	
Æ	0	0	0	1.5x10 6	1.5×10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	0	0	0	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5×10 6	
ΔC	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Δbf	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	20	-20	-20	-20	-20	-20	-20	-20	-20	20 -20	
ΛθΙν	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	20	20	20	20	20	20	20	20	20	
h/L K Data Aelv Abf	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	
Beta Beginning h/l	0.111	0.1112	0.1112	0.1368	0.1112	0.3627	0.3608	0.111	0.1368	0.1256	0.1373	0.1373	0.112	0.36	0.3894	0.113	0.1369	0.111	0.111	0.111	0.111	0.376	0.137	0.1369	0.1112	0.3812	288=125%
Beta	0	0	0	0	0	0	0	0	0	0	0	0	0	0	٥	0	0	0	0	0	0	0	0	0	0	0	
Alpha	0	0	0	4	0	4	4	0	4.	0	4.	4.	0	4	4	0	4.	0	0	0	0	4	4	4.	0	4	% 228=100%
PBEL	168	227	288	288	288	288	228	228	228	228	228	168	168	168	0	0	0	169	228	290	290	290	290	228	228	228	168=75%
o	0	0	0	9	09	09	09	09	09	9	9	9	9	9	9	09	9	0	0	0	09	9	09	09	9	09	
Date	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	2-Mar	5-Mar	5-Mar	5-Mar	5-Mar	5-Mar	5-Mar	5-Mar	5-Mar	5-Mar	5-Mar	5-Mar	5-Mar	5-Mar	5-Mar	5-Mar	5-Mar	5-Mar	
End Time	20:15	20:36	20:55	21:14	21:40	22:07	22:17	22:45	23:02	14:46	14:59	15:14	15:35	15:46	15:58	16:18	16:34	18:40	18:57	19:19	19:41	19:51	90:02	21:42	22:03	22:15	
Start Time End Time	19:57	20:20	20:40	21:00	21:21	21:58	22:10	22:23	22:50	14:25	14:47	13:03	15:19	15:40	15:51	16:04	16:23	18:22	18:41	19:02	19:23	19:45	19:56	21:32	21:47	22:08	
Run *	220	221	222	223	224	225	226	227	228	229	230	231	232	233	234	235	236	237	238	239	240	241	242	243	244	245	

Table 2 NAPF-1 NASA/Langley 14 x 22 Run Log

Gear Comments						SBE Did not go to tape	10° Body Flap runs NPR-75%	NPR=100%	NPR-125%	O=60		HGT 22.134	HGT 22.184	Came down to change tape							Repeat of Run 264	Static run Elevon Effectiveness			Elevon +20°		AJH
	5	6	6	5	6	5	8	8	8	8	6	8	6	8	6	5	8	6	8	6	6	ю	5	8	8	6	
F.F.	5	5		5	8	5	8	5	8	5	6	8	8	6	6	6	6	6	8	6	6	6	6	6	6	no	
Æ	1.5×10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5×10 6	0	0	0	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5×10 6	1.5x10 6	0	0	0	1.5x10 6	1.5x10 6	
ΔC	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
νΔbf	-20	-20	-20	-20	-20	-20	9	9	9	9	10	10	10	10	9	10	10	10	10	9	9	0	0	0	0	0	
аде	20	20	20	20	20	20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	20	20	20	20	20	
h/LK Data Aelv Abf	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	
Beta Beginning h/	0.3786	0.1109	0.1374	0.1368	0.1114	0.3879	0.1095	0.1109	0.1109	0.137	0.1203	0.3689	0.3697	0.1112	0.137	0.137	0.1111	0.3813	0.3813	0.111	0.1369	0.111	0.1115	0.111	0.1368	0.1109	288=125%
Beta	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Alpha	4	0	4.	4.	0	4	0	0	٥	4	0	4	4	0	4.	4-	0	4	4	0	4	0	0	0	4.	0	% 228-100%
PBEL	168	168	168	0	0	0	168	230	290	290	288	288	227	227	228	168	168	168	0	0	0	168	228	288	288	288	168=75%
a	9	60	60	60	9	9	0	0	0	9	60	9	09	9	9	9	9	09	09	09	9	0	0	0	09	09	
Date	5-Mar	5-Mar	5-Mar	5-Mar	5-Mar	6-Mar	6-Mar	6-Mar	6-Mar	6-Mar	6-Mar	6-Mar	6-Mar	6-Mar	6-Mar	6-Mar	6-Mar	6-Mar	6-Mar	6-Mar	6-Mar	6-Mar	6-Mar	6-Mar	6-Mar	6-Mar	
End Time	22:25	22:47	23:03	23;19	23:38	9:23	11:57	13:43	14:14	14:30	14:58	15:17	15:19	15:41	16:49	17:07	17:27	17:45	17:58	18:19	18:37	20:35	20:56	21:17	21:38	22:02	
Start Time End Time	22:20	22:30	22:53	23:08	23:24	9:16	11:43	13:28	13:53	14:20	14:37	15:01	15:18	15:23	16:37	16:55	17:10	17:38	17:51	18:03	18:24	20:15	20:40	21:03	21:27	21:44	
Run #	246	247	248	249	250	251	252	253	254	255	256	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	

Table 2 NAPF-1 NASA/Langley 14 x 22 Run Log

																											1
Gear Comments				Wind on at 21:23 HMELV 2.4 inlbs	HGT check Elevon Effectiveness Runs ELEV=20°						Elevon -20°								Height corrected		Height Check, New Tape					Static Runs ELEV -10°	A.H.
Gea	6	8	6	6	6	5	6	6	8	6	5	6	5	6	6	6	6	6	8	6	5	6	6	6	5	6	
H.	6	6	6	6	8	5	8	5	8	6	6	6	6	6	6	6	Po	6	6	e e	8	5	5	8	6	6	
Æ	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	0	0	0	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5×10 6	0						
δ¢	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
ΛΔbf	0	0	0	0	0	0	0	0	0	٥	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
a Ael	20	20	20	20	20	20	20	20	20	20	-20	-20	-20	-20	-20	-20	-20	-20	-20	-20	-20	-20	-20	-20	-20	-10	
LK Dat	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	
Beta Beginning h/L K Data Aelv Abf	0.3695	0.3695	0.111	0.1368	0.137	0.1111	0.3797	0.137	0.1108	0.3655	0.1105	0.11	0.1113	0.1374	0.1112	0.3583	0.3566	0.1108	0.1369	0.1369		0.3915	0.3887	0.1109		0.111	288=125%
Beta	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Alpha	4	4	0	4.	4.	0	4	4	0	4	0	0	0	4.	0	4	4	0	.4	4-	0	4	4	0	4-	0	100
PBEL	288	228	228	228	168	168	168	0	0	0	168	226	288	288	288	290	229	228	228	168	168	168	0	0	0	168	168=75%
σ	9	09	9	09	09	09	09	9	9	09	0	0	0	60	9	60	60	90	9	90	90	90	09	9	09	0	
Date	6-Mar	6-Mar	6-Mar	6-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	
End Time	22:13	22:26	22:46	23:01	8:40	90:6	9:20	9:39	10:03	10:16	12:12	13:32	13:54	14:14	14:35	14:45	14:59	15:18	16:02	16:16	16:38	17:51	18:02	18:26	18:40	20:42	
Run # Start Time End Time	22:08	22:18	22:29	22:51	8:27	8:45	9:12	9:56	9:44	10:09	11:50	13:11	13:37	14:03	14:19	14:39	14:52	15:03	15:57	16:05	16:21	17:45	17:56	18:08	18:29	20:25	
Run #	272	273	274	275	276	277	278	279	280	281	282	283	284	285	286	287	288	289	290	291	292	293	294	295	296	297	

Gear Comments										New height procedure						Static runs ELEV10° Measure elevon at alpha 0° (see notes)				No Kulite data, regular running	HGT update (no good)			HGT update (no good)		Came down to change tape	HV
Gear	8	6	8	6	8	8	8	8	8	8	6	8	8	8	6	5	5	5	5	6	5	5	5	8	5	5	
F.F.	6	o	O	6	6	6	6	8	8	5	O	6	8	6	6	6	5	5	5	5	6	5	5	6	5	5	
Æ	0	0	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5×10 6	1.5×10 6	1.5x10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5x10 6	1.5x10 6	0	0	0	1.5x10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5x10 6	1.5×10 6	1.5×10 6	
ΔC	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
Δbf	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
аде	-10	-10	-10	-10	-10	-10	-10	•10	-10	-10	-10	-10	-10	-10	10	10	0	10	10	10	10	10	10	10	9	10	
h/L K Data Aelv Abf	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	Yes	2	2	2	2	2	2	2	
Beta Beginning h/	0.1208	0.1113	0.111	0.137	0.3658	0.3658	0.111	0.1367	0.1367	0.111	0.3874	0.3887	0.111	0.137	0.111	0.111	0.111	0.3846	0.1106	0.1377	0.37	0.111	0.1371	0.3628	0.111	0.1368	288-125%
Beta	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
Alpha	0	0	0	4.	4	4	0	4	7	0	4	4	0	4.	0	0	0	4	0	4	4	0	4.	4	0	4.	% 228-100%
PBEL	228	288	288	288	288	228	228	228	168	168	170	0	0	0	170	228	289	288	287	287	229	229	229	168	170	169	168-75%
o	0	0	09	60	9	9	9	9	60	9	60	09	9	9	0	0	0	9	9	60	9	60	9	9	9	09	
Date	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	7-Mar	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	
End Time	21:08	21:32	21:55	22:12	22:26	22:36	22:55	23:12	23:26	8:20	9:10	9:20	9:46	10:01	11:35	11:48	13:05	13:46	14:12	14:32	14:41	15:01	15:18	15:31	15:50	16:08	
Run # Start Time End Time	20:51	21:14	21:40	21:59	22:20	22:27	22:40	23:00	23:15	7:45	8:55	9:14	9:25	9:50	11:15	11:37	11:50	13:07	13:51	14:17	14:35	14:45	15:06	15:24	15:35	15:57	
Run #	298	299	300	301	302	303	304	305	306	307	308	309	310	311	312	313	314	315	316	317	318	319	320	321	322	323	

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				1				1																		7	
Gear Comments				Landing Gear off	off Config. # changed for 4° beta	off kulite hgt's: 6.6",7.8".9.6",15",45"	config. # change		Static runs	Static runs	Static runs HGT 6.2910	off Mast lower HGT=5.8520, Repeat of Run 331	off Mast lower HGT=5.448	Mast lower HGT=4.9422	off Mast lower HGT=4.7063	Sidewalls Off Static Runs			kulite hgt's: 6.6",7.8".9.6",15",24",45"					Coming Down for tape rewind			AJH
Gear	6	8	8	10	9	9	10	9	9	off	9	9	off	10	off	8	8	6	8	6	5	6	5	5	5	6	
<u>n</u>	6	6	8	5	5	8	5	6	8	8	6	5	5	5	5	9	9	50	off	off	9	off	=	9	off	off	
Æ	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5×10 6	1.5x10 6	0	0	0	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	0	0	0	1.5x10 6	1.5×10 6	1.5x10 6	1.5×10 6	1.5×10 6	1.5x10 6	1.5×10 6	1.5×10 6	
δС	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
νΔbí	0	0	0	٥	0	0	0	0	0	0	٥	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
tabel	2	2	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0 8	
/LK Da	2	2	2	Yes	Yes	Yes	Yes	Yes	2	2	2	2	2	2	2	2	2	2	, Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	
Beta Beginning h/LK DataΔelv Δbf	0.1368	0.1109	0.3862	0.1106	0.1106	0.1109	0.1109	0.1109	0.1109	0.1109	0.1048	0.0975	0.0908	0.08237	0.07844	0.111	0.111	0.1102	0.137	0.11	0.39	0.392	0.1105	0.1372	0.1372	0.1105	288=125%
Beta	0	0	0	0	4	4	0	0	0	0	0	0	4	4	0	0	0	0	0	0	0	0	0	0	0	0	
Alpha	4.	0	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4.	0	4	4	٥	4	4.	0	% 228-100%
PBEL	0	0	0	168	168	228	228	288	288	228	168	288	288	0	0	168	228	288	288	288	288	228	228	228	168	168	168-75%
σ	9	60	60	60	60	9	9	9	0	0	0	09	9	9	9	0	0	0	9	09	09	9	9	9	09	09	
Date	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	8-Mar	9-Mar	9-Mar	9-Mar	9-Mar	9-Mar	9-Mar	9-Mar	9-Mar	9-Mar	9-Mar	9-Mar	9-Mar	9-Mar	9-Mar	9-Mar	9-Mar	
End Time	17:20	17:42	17:53	21:10	21:34	22:01	22:24	22:55	23:16	23:34	8:47	9:14	9:37	10:00	10:26	10:55	13:26	13:54	14:09	14:33	14:52	15:02	15:28	15:48	17:19	17:46	
Start Time End Time	17:09	17:25	17:47	20:54	21:12	21:39	22:05	22:30	22:57	23:19	8:30	8:55	9:19	9:43	10:07	10:28	13:10	13:31	13:59	14:11	14:38	14:58	15:04	15:34	16:54	17:22	
Run *		325	326	327	328	329	330	331	332	333	334	335	336	337	338	339	340	341	342	343	344	345	346	347	348	349	

Table 2 NAPF-1 NASA/Langley 14 x 22 Run Log

			-		-						-	_				-	-			-		-		-			1
Gear Comments			Kulite data stopped at h/l 0.4007	Last Run before knuckle change	alpha 14° Baseline Static Runs			23 min run time, Repeat of Run 124	20 min run time	15 min run time	25 min run time	Got first 4 points, then tape ran out!	Repeating Run 361	on Continue with Baseline runs, Repeat of Run 123	Repeat of Run 96					24° Knuckle Baseline, Repeat of Run 95	24° Knuckle Baseline	24° Knuckle Baseline	24° Knuckle Baseline	Checked Height	Ran Out of Tape	Repeat of Run 374	A IM
	5	5	5	8	5	5	6	8	8	5	6	6	8	5	8	8	8	8	5	5	8	5	5	5	5	6	
F.F.	off	off	off	off	6	6	6	8	6	8	6	o	8	8	6	8	6	8	8	8	8	8	5	5	8	6	
Æ	1.5×10 6	1.5×10 6	1.5×10 6	1.5x10 6	0	0	0	1.5x10 6	1.5x10 6	1.5x10 6	1.5×10 6	1.5x10 6	1.5x10 6	1.5×10 6	1.5×10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5×10 6	1.5x10 6	1.5×10 6	
ρc	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
Δbf	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
аде	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	٥	0	0	0	0	0	0	0	0	0	
NLK Data Aelv Abf A c	Yes	Yes	Yes	2	2	2	2	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	2	2	2	2	2	2	2	
Beta Beginning h/l	0.3823	0.3804	0.1105	0.1372	0.0417	0.0417	0.0417		0.04377	0.06785	0.06702	0.04356	0.043	0.05	0.0514	0.0439	0.06752	0.067	0.043	0.05	0.05073	0.04365	0.06674	0.067	0.04352	0.04352	288-125%
Beta	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4	4	4	4	4	4	1
Alpha	4	4	0	4.	14	14	14	12	4	16	16	14	14	12	12	14	16	16	14	12	12	14	16	16	4	14	1
PBEL	168	0	0	0	168	228	288	288	288	288	228	228	228	228	168	169	168	0	0	0	0	0	0	168	168	168	168-75%
o	90	60	60	60	0	0	0	90	9	60	9	60	90	9	60	90	9	9	9	9	9	9	09	09	09	09	
Date	9-Mar	9-Mar	9-Mar	9-Mar	12-Mar	12-Mar	12-Mar	12-Mar	12-Mar	12-Mar	12-Mar	12-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	
End Time	18:01	18:15	18:41	18:57	17:15	17:30		21:18	21:47				8:31	8:59	9:56	9:56	10:25	11:27	11:55	13:13	13:35	13:54	14:14	14:47	15:10 13-Mar	16:39	1
Start Time End Time	17:53	18:07	18:20	18:46	17:01	17:16	17:36	20:55	21:26	21:54	22:16	22:42	8:10	8:33	9:03	9:30	10:01	11:00	11:30	12:53	13:22	13:40	14:00	14:35	14:52	16:21	
Run #	350	351	352	353	354	355	356	357	358	359	360	361	362	363	364	365	366	367	368	369	370	371	372	373	374	375	

168-75% 228-100% 288-125%

Table 2 NAPF-1 NASA/Langley 14 x 22 Run Log

Gear Comments	6	on Repeat of Run 135	uo	uo	uo	CO	on Tunnel Down and off for Model Change, Repeat of Run 134	on Body Flap =10°, Static Run, BF not Gaged	on Q-60 Min. height is 3"	on Time includes ESP calabration 22 minutes	on Time includes ESP calabration 17 minutes	wo	on Time includes ESP calabration	vo	uo	uo	uo	on Pressure Check Out Run - Fixed CW, Throat Area, & CTI	vo	uo	uo	on +20° Body Flap, Static Run, Wrong HMBF Constant	on Wrong HMBF Constant -Will correct on tape	on Wrong HMBF Constant -Will correct on tape	on Wrong HMBF Constant -Will correct on tape	on Wrong HMBF Constant -Will correct on tape	AJH
n.	U0	o	O	ou	O	uo	uo	O	6	no	O	on	no	O	o	ou	o	6	uo	ou	uo	LO	LO	Lo	6	6	
Æ	1.5x10 6	1.5x10 6	1.5×10 6	1.5x10 6	1.5×10 6	1.5x10 6	1.5x10 6	0	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5×10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5×10 6	1.5×10 6	0	1.5×10 6	1.5x10 6	1.5×10 6	1.5×10 6	
ΔC	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Δbf	0	0	0	0	0	0	0	10	0	10	10	10	10	10	10	10	10	10	10	10	10	20	20	20	20	20	
Δelv	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
h/LK Data Aely Abf	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	
Beta Beginning h/l	0.05022	0.06041	0.04388	0.06688	0.06688			0.4	0.05003	0.04986	0.0668	0.0668	0.0525	0.05013	0.0605	0.05128	0.06666	0.3998	99990.0	0.0512	0.05	0.05	0.05	0.05	0.06658	0.06741	288-125%
Beta	4	4	4	4	4	4	4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-1	
Alpha	12	12	14	16	16	14	12	14	14	12	16	16	14	12	12	14	16	1216	16	4	12	14	14	12	16	- 1	6 228-100%
PBEL	168	228	228	228	288	288	288	228	288	288	288	228	228	228	168	168	168	168-288	0	0	0	228	288	288	288	228	168-75
o	9	60	60	60	60	9	9	0	09	9	60	60	9	9	9	60	60	09	09	9	60	0	9	09	09	09	
Date	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	13-Mar	14-Mar	14-Mar	14-Mar	14-Mar	14-Mar	14-Mar	14-Mar	14-Mar	14-Mar	14-Mar	14-Mar	14-Mar	
nd Time	16:54	17:25	17:45	18:02		19:04	19:20	21:13	-	21:52	22:08	22:42	23:00	23:17	8:13		8:48	10:44	11:00	11:17	11:33				14:05	14:21	
Start Time End Time	16:41	17:00	17:29	17:51	18:32	18:47	19:07	21:12	21:19	21:35	21:53	22:31	22:43	23:03	8:03	8:18	8:36	10:27	10:49	11:05	11:22				13:53	14:10	
Run *	376	377	378	379	380	381	382	383	384	385	386	387	388	389	390	391	392	393	394	395	396	397	398	399	400	401	

Gear Comments	on Wrong HMBF Constant -Will correct on tape	Updated HMBF Constant, Repeat of Run 402		Height Check, off by 0.8 inches					Height Check, off by 0.3 inches	ESP Calibration, Changes HMBF Constants	Baseline Check	Baseline Check	Repeat of run 368	Repeat of run 362	Repeat of run 360	Repeat of run 358	BFE Static Run -20°	Body Flap Effectiveness			Height Check, off 1 inch, corrected	Hgt 3.065", Repeat of Run 420		Height Check, off 1.6 inches, corrected			HCA
Gear	8	8	8	8	5	5	8	5	5	8	5	5	5	8	5	8	5	5	5	8	8	8	8	8	8	6	
H.	8	6	8	6	8	8	8	8	8	8	6	6	6	6	6	6	6	6	6	6	8	6	6	8	8	6	
Æ	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5×10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5×10 6	1.5x10 6	1.5x10 6	1.5×10 6	1.5x10 6	٥	1.5×10 6	1.5×10 6	1.5×10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5×10 6	1.5x10 6	1.5x10 6	
ρc	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Abf	20	20	20	20	20	20	20	20	20	0	0	0	0	0	0	0	-20	-20	-20	-20	-20	-20	-20	-20	-20	-20	
a del	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	٥	0	0	0	0	0	
h/L K Data selv abf	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	
Beta Beginning h/l	0.05		0.05081	0.05081	0.06728		0.06045	0.060215	0.080449	0.9847	1.003	0.9858	0.06008	0.06008	0.0606			0.0503	0.06045	0.06761	0.06007	0.05109	0.06774	90090.0			288-125%
Beta	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
Alpha	7	14	12	12	16	1	12	7	16	1216	16-12	1216	1	1	16	1	14	12	14	16	12	14	16	12	41	16	Ι
PBEL	228	228	228	168	168	168	0	0	0	168	228	288	0	228	228	288	228	228	228	228	288	228	288	168	168	168	168-75%
o	9	9	9	60	60	9	90	60	60	9	60	60	60	60	60	9	0	9	9	9	9	9	9	9	09	09	
Date	14-Mar	14-Mar	14-Mar	14-Mar	14-Mar	14-Mar	14-Mar	19:45 14-Mar	14-Mar	14-Mar	14-Mar	14-Mar	14-Mar	14-Mar	14-Mar	14-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	
End Time		17:13	17:35	18:24		18:58		19:45	19:58	21:23	21:34	21:44	_	22:31	22:47	23:05		8:44	9:01	9:19	9:36	9:54	10:11	10:40	10:57	11:12	1
Start Time End Time	14:20	17:00	17:16	18:05	18:28	18:47	19:15	19:27	19:47	21:18	21:28	21:35	21:59	22:16	22:33	22:52	8:25	8:30	8:49	9:07	9:23	9:38	9:59	10:20	10:40	11:00	
Run *		403	404	405	406	407	408	409	410	411	412	413	414	415	416	417	418	419	420	421	422	423	424	425	426	427	

168-75% 228-100% 288-125%

Table 2 NAPF-1 NASA/Langley 14 x 22 Run Log

Gear Comments	uo	uo	uo	on Height Check, off 1.4 inches, corrected	uo	uo	uo	uo	uo	on Height Check, off 1.5 inches, corrected, Noticed HMELV off scale	uo	on Taps S6,14,9 were plugged	ю	on Hgt check, off 0.5", corrected Fixed HMELV	uo	uo	on Static Run for Elevon -20°	uo	uo	uo	on Hgt check, off by 1.1", corrected	uo	on Height corrected	uo	on hgt corrected, off by 0.6" Tunnel down & off	on checked hgt before blow, off by 1.4", corrected	1
n.	6	6	6	6	6	6	8	6	6	o	6	ou	6	0	6	ю	6	6	6	6	6	6	6	LO CO	uo l	uo	
Æ	1.5x10 6	1.5×10 6	1.5x10 6	0	1.5x10 6	1.5×10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	1.5x10 6	0	1.5×10 6	1.5x10 6	1.5×10 6	1.5x10 6	1.5x10 6	1.5×10 6	1.5x10 6	1.5×10 6	1.5×10 6	
ρ	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Δbf	-20	-20	-20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Δelv	0	0	0	20	20	20	20	20	20	20	20	20	20	20	20	20	-20	-20	-20	-20	-20	-20	-20	-20	-20	-20	
h/LK Data Aelv Abf	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	
Beta Beginning h/	0.0608				0.06043	0.0512	0.0677	0.0615	0.0518	0.0678	0.0603	0.0504	0.0679	0.08051	0.0504		0.05	0.06009		0.0674	0.06028	0.05048	0.06699		0.0524	0.05996	288-125%
Beta	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Alpha	12	41	16	14	12	14	16	12	4	16	12	14	16	12	4	16	41	12	14	16	12	4	16	16	14	12	% 228-100%
PBEL	0	0	0	228	228	228	228	0	0	0	288	288	288	168	168	168	228	230	228	230	288	288	288	168	168	168	168-75%
o	60	60	60	0	60	90	9	9	60	60	60	9	9	9	60	9	0	9	9	9	9	9	9	9	9	9	
Date	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	22:28 15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	15-Mar	20:40 15-Mar	
End Time	11:28		11:50	13:46	13:58	14:13	14:26	14:46	15:08	17:26	17:49	_	18:24	19:22	19:39	20:00	21:34	21:52	22:15	22:28	23:15	23:33	16:06	16:22	20:19	20:40	
Start Time End Time	11:14	11:31		13:45	13:49	14:02	14:17	14:32	14:51	17:12	17:33	17:55	18:13	19:06	19:24	19:42	21:15	21:39	21:54	22:17	23:05	23:20	15:53	16:13	20:08	20:20	
Run *	428	429	430	431	432	433	434	435	436	437	438	439	440	441	442	443	444	445	446	447	448	449	450	451	452	453	

Table 2 NAPF-1 NASA/Langley 14 x 22 Run Log

Gear Comments			Measured elevon at -20.6° for left & right	Hgt check, off 1",, run includes weight tares	Elevon -10°			Hgt check, off 0.9", corrected			Elevon measured at 10.2°-right, 10.6°-left hgt off by 0.9"				Hgt check off by 1.2"			Static Run Body Flap -10°			Hgt check off by 0.7", corrected	Run Number skipped		Hgt check off by 0.9", corrected			HCA
Gear	8	8	8	6	5	8	8	8	8	8	8	8	8	8	6	6	6	5	8	5	5		8	6	6	o	
F.F.	8	8	8	8	5	8	8	8	8	8	5	8	8	5	8	6	6	8	8	5	8		8	6	6	o	
Æ	1.5×10 6	1.5×10 6	1.5×10 6	0	1.5×10 6	1.5×10 6	1.5x10 6	1.5×10 6	1.5×10 6	1.5×10 6	0	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5x10 6	0	1.5×10 6	1.5x10 6	1.5×10 6		1.5×10 6	1.5x10 6	1.5x10 6	1.5×10 6	
ΔC	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		0	0	0	0	
Abi	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-10	-10	-10	-10		-10	-10	-10	-10	
аде	-20	-20	-20	-10	-10	-10	-10	-10	-10	-10	9	10	9	-	-	-	10	0	0	٥	0		0	0	0	0	
h/LK Data Aelv Abf	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2		2	2	2	2	
Beta Beginning h/		0.0524		0.05141	0.05141		0.0801	0.06106	0.05061	0.06682	0.9924	0.05038	0.06844	0.0608							0.06023		0.06023	0.05022	0.06713	0.06713	288=125%
Beta	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		0	0	0	0	
Alpha	12	14	16	14	14	16	12	12	14	16	14	14	16	12	12	14	16	14	14	16	12		12	14	16	16	6 228-100%
PBEL	0	0	0	227	227	227	227	0	0	0	228	228	228	228	0	0	0	228	228	228	228		288	288	288	168	168-75%
o	9	9	60	0	9	9	9	9	9	9	0	9	9	9	9	9	60	0	9	9	9		9	9	9	60	
Date	15-Mar	15-Mar	15-Mar	19-Mar	19-Mar	19-Mar	19-Mar	19-Mar	19-Mar	19-Mar	19-Mar	19-Mar	19-Mar	19-Mar	19-Mar	19-Mar	19-Mar	19-Mar	19-Mar	19-Mar	19-Mar		19-Mar	19-Mar	19-Mar	19-Mar	
End Time	21:27	21:50	_		14:12	14:29	14:45	15:18	15:43	15:57	16:52	17:06	17:32	17:48	18:08	18:26	18:44	20:11	20:30	20:45	21:05		21:24	0:00	22:03	22:21	
Start Time End Time	21:16	21:32	21:53	13:29	13:48	14:12	14:31	15:00	15:24	15:44	16:50	16:53	17:12	17:35	17:50	18:18	18:29	20:02	20:14	20:33	20:53		21:09	21:31	21:50	22:08	
Run *	454	455	456	457	458	459	460	461	462	463	464	465	466	467	468	469	470	471	472	473	474	475	476	477	478	479	

Table 2 NAPF-1 NASA/Langley 14 x 22 Run Log

Gear Comments			After up on screen HGT=3.567, should be 6", corrected, M.F.			Min. height 4" w/Speed Brake			model change-sidewalls off, elevons 0°, Body flap 0°	Sidewall Effectiveness										Started Kulite data			off Landing Gear off Static Run				AJH
Gear	8	6	8	6	6	6	8	ь	6	6	6	G _O	6	o G	6	6	e o	6	6	6	6	ou	off	off	110	off	
F.F.	6	6	8	6	6	6	6	6	6	off	off	off	off	off	off	off	011	off	off	off	off	011	no	6	0	6	
Æ	1.5x10 6	1.5x10 6	1.5×10 6	1.5x10 6	1.5×10 6	0	1.5x10 6	1.5x10 6	1.5x10 6	0	1.5×10 6	1.5x10 6	1.5x10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5x10 6	1.5×10 6	1.5×10 6	0	1.5×10 6	1.5×10 6	1.5×10 6	
ΔC	0	0	0	0	0	0	0	0	0	۰	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
νΔbί	-10	-10	-10	-10	-10	-20	-20	-20	-20	٥	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
аде	0	0	0	0	0	20	20	20	20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
h/L K Data delv dbf	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	2	Yes	Yes	Yes	Yes	Yes	Yes	Yes	
Beta Beginning h/	0.0544	0.0607	0.0602	0.05023		0.06667		0.0517	0.0141	0.05094	0.05039				0.05106						0.05026	0.05026					288=125%
Beta	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
Alpha	4	12	12	14	16	0	12	4	16	4	14	12	16	16	14	12	12	4	16	16	14	12	14	14	16	12	
PBEL	168	168	0	0	0	0	0	0	0	228	228	228	228	288	288	288	168	168	168	0	0	0	228	228	228	228	168-75%
σ	9	9	09	9	09	0	09	9	9	0	9	09	9	9	09	9	9	9	9	09	9	09	0	9	09	9	
Date	19-Mar	19-Mar	19-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	
End Time	22:41	23:00	-	_		10:05	10:20	10:40	11:00	13:14										17:00		17:36	18:27	18:45	19:01	19:22	1
Start Time End Time	22:22	22:46	23:05	8:00	8:20	9:50	10:06	10:26	10:45	13:04	13:15	13:34	13:52	14:15	14:27	14:50	15:07	15:45	16:50	17:04	17:15	17:38	18:00	18:30	18:49	19:06	
Run *	480	481	482	483	484	485	486	487	488	489	490	491	492	493	494	495	496	497	498	499	200	501	505	503	504	505	

Table 2 NAPF-1 NASA/Langley 14 x 22 Run Log

Gear Comments				Static Run	Beta Sweep to 8° Yaw out of ground effect	Beta Sweep to 8° Yaw in ground effect, hgt check, off 1.4"	Alpha sweep at PBEL 312	Increased PBEL	Increased PBEL	PBEL sweep	HGT Check OK, Repeat of Run 355	Repeat of Run 361	Repeat of Run 360		Repeat of Run 378	Repeat of Run 371						Control of the Contro	АЛН
Gear	-	9	9	8	5	8	5	8	5	8	6	8	5	6	8	8	6						
n.	6	0	8	6	6	6	8	6	8	6	6	6	LO .	e	G	6	6						
Æ	1.5×10 6	1.5×10 6	1.5×10 6	0	1.5×10 6	1.5×10 6	1.5×10 6	1.5×10 6	1.5x10 6	0	0	1.5×10 6	1.5×10 6	1.5×10 6	1.5x10 6	1.5x10 6	1.5x10 6						
ΔC	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0						
Δbf	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0						
la Ael	0	0	0	٥	0	0	0	0	0	0	0	0	0	0	0	0	0				_		
h/LK Data aelv abf	Yes	Yes	, Yes	2	2	2	2	2	2	2	2	2	2	2	2	2	2						
Beta Beginning h/				0.75	0.75	0.05026	0.9902	-	0.9878	-						0.06052	0.06139						288=125%
Beta	0	0	0	0	0-8	8-0	0	0	0	0	0	0	0	0	4	4	0						1
Alpha	12	14	16	14	4	4	1216	16-12	1216	14	14	14	16	10	4	14	10						% 228-100%
PBEL	0	0	0	228	228	228	312	342	375	375-312	228	228	228	228	228	0	0						168=75%
σ	90	60	60	0	60	9	9	9	9	0	0	9	9	60	9	60	60						
Date	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	20-Mar	21-Mar	21-Mar	21-Mar	21-Mar	21-Mar	21-Mar	21-Mar	21-Mar	21-Mar	21-Mar	21-Mar	21-Mar					
End Time	19:41	19:58	_		22:15	22:35	9:52	9:59	10:16	10:27	10:57	11:10	11:30	13:02	13:22								
Start Time End Time	19:26	19:45	20:01	21:56	22:00	22:19	9:43	9:53	10:07	10:19	10:33	10:59	11:12	12:58	13:08	13:27	13:46	13:57					
Pen *		507	508	509	510	511	512	513	514	515	516	517	518	519	520	521	522	EOT					

Table 3

Date	Run Number	Comment
2/22	95 - 101	ESP voltage regulator problem
2/23	108 - 109 (between)	Installed Pt / Ps rake
2/23	109 - on	ESP reference to P∞
2/23	111	Balance voltage dropped, ESP's did not calibrate, voltage regulator broke (run 112 was a repeat of run 111) Fixed at 8:45 pm
2/26	120	ESP channels 1 through 96 read 14.98 while channels 97 through 160 read 14.62
2/26	128	At the end of the run 1 - 96 read 14.96 while 97 - 160 read 14.61 and the Rusko read 15.12
2/27	139	All ESP's calibrated to 14.97, while the Rusko read 15.059 psi
2/27 in the aft	ternoon	Repeated runs for kulite data, the kulite data was bad due to the MODCOMP
2/27	158	ESP numbering was incorrect due to ESP interface hookup error.
2/28 9:15 am	173	ESP's calibrate fine, but suspect a pinched line, ESP numbering problem resolved, Began running Body Flap deflections of -20°
2/28 6:15 pm	before 177	Applied pressure to ESP reference line, pressures 1 through 96 did not change, but 97 through 160 did. Found a pinched line in reference line for 1 through 3.
2/28 8:50 pm	177	Wyle Co. fixed offset problem in ESP readings (0.1 psi) Rusko read 14.898, ESP 18.84. Channels 97 to 160 where drifting
3/1	181	Reference line run check out OK, ESP ref, changed to PA.
3/2		Body Flap runs were bad, BFHM channel was moved late Friday afternoon
3/2	210-228	HMBF was hooked into wrong channel on electric panel

NASP COMPETITION SENSITIVE ROCKWELL INTERNATIONAL CORPORATION ROCKETDYNE

Table 3

Date	Run Number	Comment
3/5		Found open body flap gage down stairs on the electric channel board. By 9 am the body flap and elevon were fixed
3/6	251	This run did not go on to the magnetic tape
3/6 11:25 am	252	Changed elevon and body flap tygon pressure tap jumpers
3/12		Knuckle change from 0° to 24°
3/12		Moved 24° knuckle forward of roll coupler
3/12 2:05 pm		Checked body Flap and elevon pressure taps and they looked good. Checked reference lines and they looked good
3/12 7:00 pm		Suspected pinched lines in forward, nose, ESP. Used bellows to check reference lines and it looks good
3/14 9:00 am		Found reference lines 1-3 pinched
3/14 10:15 an	1	Checked ESP reference lines and they are good
3/14 2:55 pm		Nose ESP out putting bad data, we believe this due to heat.
3/14	397-402	HMBF constants were incorrect
3/9		Kulite run, one half of run 352 and 353, no Kulite data was obtained.
3/13 5:10 pm		PBEL read 6 psi and PSTING read 800 psi, this was due to an open vent
3/13	397-402	Body Flap constants set for 0°
3/13	403	Body Flap constant changed
3/15	437-440 (6:00 pm)	Bad HMELV reading
3/15 6:55 pm		Unplugged and replugged elevon gage, now working
3/15 8:00 pm	437-440	Tape was left on taps \$6,14 and \$6,9

		Table 3
Date	Run Number	Comment
3/16 7:00 am	before 457	Found condensation on model, water was completing a connection between the grounding strip and the metric part of the model.
3/16 7:30 am		Pressure lines were inadvertently melted and resulted in model break down.
3/16 3:00 pm		Model was reassembled and checked out OK. Connected channels 59, 90, & 128 to the ESP reference line manifolds.
3/16 7:00 pm		Found a calibration line crimped in the strut cover
3/16 8:40 pm		Found another crimped ESP line
3/16 9:15		Check out ESP Calibration - OK
3/19	before 457	ESP problems with pressures 1-96, reference line cut by strut fairing. Removed strut fairing, protected instrumentation lines with tape.
3/19	457-470	Runs were conducted without the strut fairing
3/19 7:00 pm		Strut fairing was grounded out and placed back on the blade strut
3/20	before 489	SR5,1; SR6,2; SR6,1; SR7,1 were plugged by plaster, but SR5,1 and SR6,1 were not hooked up. The other two taps cleaned out and seem to check out.
3/20 6:30 pm	502	After removing the landing gear and readjusting the computer, the PBEL reading jumped 10 psi, from 14.33 to 24.33 psi.
3/20 9:50 pm	509	The landing gear was put back onto the model and PBEL returned to 14.33 psi.

13.0 FIGURES

Figure 1	Total Pressure Taps & Nozzle Location for NAPF-1 Model
Figure 2	Instrumentation for Internal Nozzle
Figure 3	Instrumentation Layout on NAPF-1 Aft Body
Figure 4	Model Support Set-Up at NASA/Langley 14 x 22
Figure 5	NAPF-1 Model Lift & Trim Characteristics
Figure 6	Body Flap Effectiveness at Alpha of 14° for the NAPF-1 Model
Figure 7	Body Flap Effectiveness at Alpha of -4° for the NAPF-1 Model

NASP COMPETITION SENSITIVE ROCKWELL INTERNATIONAL CORPORATION ROCKETDYNE

Front View of Flow Module - Looking Aft

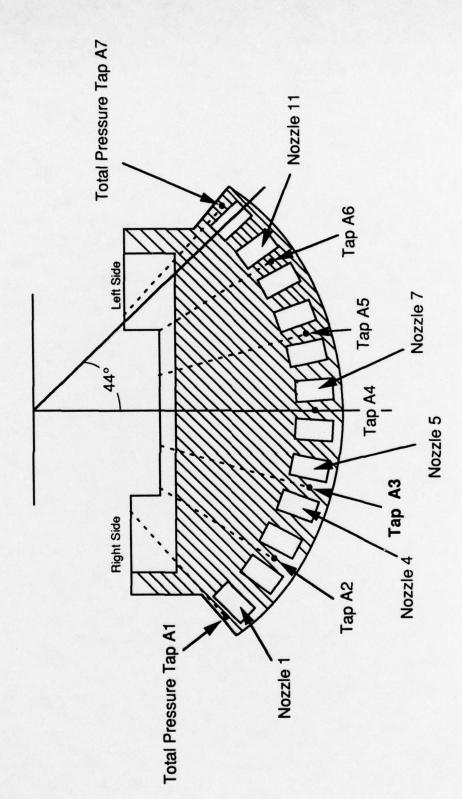
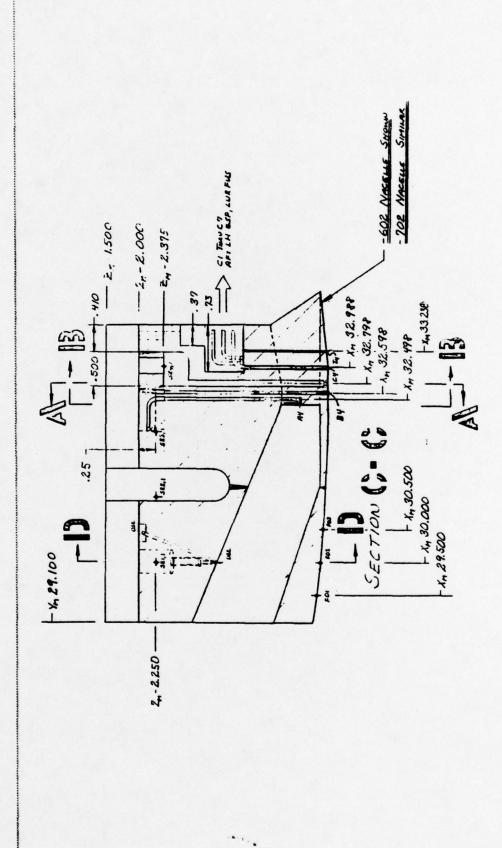


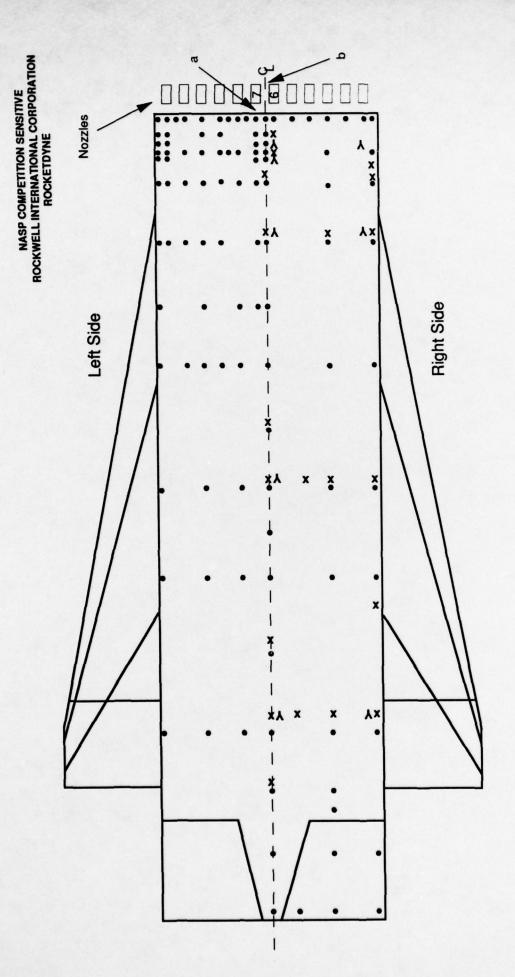
Figure 1 Total Pressure Taps & Nozzle Location for NAPF-1 Model

Figure 2 Instrumentation for Internal Nozzle (U)



UNCLASSIFIED

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Bottom View

o Static Pressure Taps x Coax Thermocouples Y Kulites

Figure 3. Instrumentation Layout on NAPF-1 Aft Body

NASP COMPETITION SENSITIVE ROCKWELL INTERNATIONAL CORPORATION ROCKETDYNE

MODEL SUPPORT SET-UP

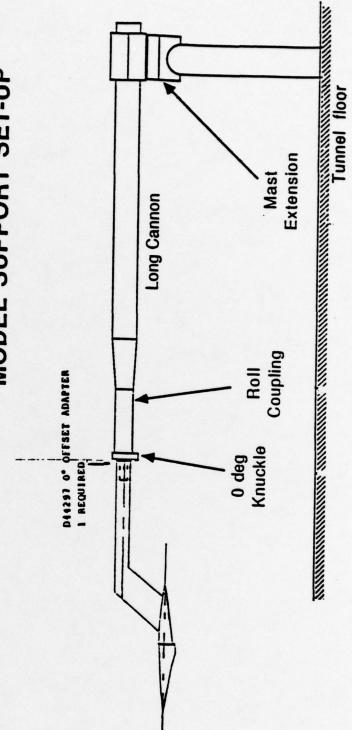


Figure 4. Model Support Set-Up at NASA/Langley 14×22

NASP COMPETITION SENSITIVE ROCKWELL INTERNATIONAL CORPORATION ROCKETDYNE

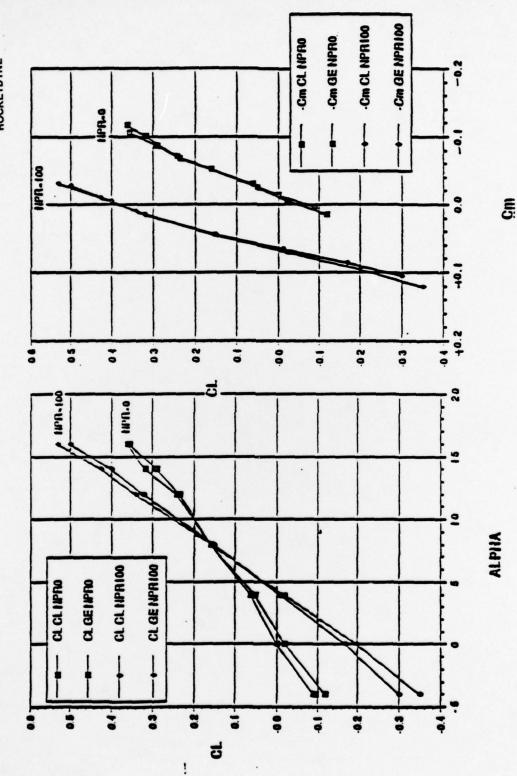


Figure 5. NAPF-1 Model Lift & Trim Characteristics

NASP COMPETITION SENSITIVE ROCKWELL INTERNATIONAL CORPORATION ROCKETDYNE

—APAS Unpowered

ONAPF-1 Unpowered

NAPF-1 Powered NA 50-147 0.37 0.1 0.0 0.2--0.1 DCm POWERED AND UNPOWERED **ELEVON EFFECTIVENESS** ALPHA= 14 0.127 0.08 0.00 0.04 900

0.47

0.3

0.2

0.1-

검

-0.0-

Figure 6. Body Flap Effectiveness at Alpha of 14° for the NAPF-1 Model

Delta Elevon

0

-10

-0.3 -0.5 -0.5

30

20

10

0

10

-20

-0.08 -30

20

10

0

-10

4. 6. 9.

-0.3 -

-0.2

0.1

Delta Elevon

-0.2

-0.04

Delta Elevon

1.5



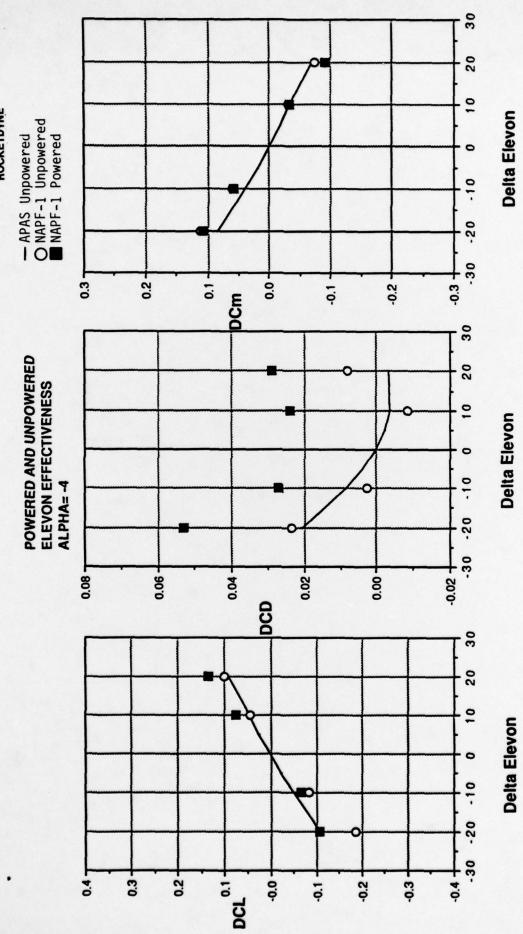


Figure 7. Body Flap Effectiveness at Alpha of -4° for the NAPF-1 Model

END

DATE .

11-94

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